

Single Event Effects (SEE) Testing of the ISL72027SEH CAN Transceiver

Introduction

The intense proton and heavy ion environment encountered in space applications can cause a variety of Single Event Effects (SEE) in electronic circuitry, including Single Event Upset (SEU), Single Event Transient (SET), Single Event Functional Interrupt (SEFI), Single Event Gate Rupture (SEGR) and Single Event Burnout (SEB). SEE can lead to system-level performance issues including disruption, degradation and destruction. For predictable and reliable space system operation, individual electronic components should be characterized to determine their SEE response. This report discusses the results of SEE testing performed on the [ISL72027SEH](#) CAN transceiver.

Product Description

The ISL72026SEH, ISL72027SEH and ISL72028SEH are a family of radiation tolerant Controller Area Network (CAN) bus transceivers. These parts are designed to meet ISO11898-2 physical layer specifications. They are fabricated in Intersil's proprietary BCD SOI process with deep trench isolation. The ISL7202xSEH parts are bond options of the same silicon die. Further description and explanation of the differences between the parts can be found in the datasheets.

Product Documentation

- [ISL72026SEH](#) datasheet
- [ISL72027SEH](#) datasheet
- [ISL72028SEH](#) datasheet
- Standard Microcircuit Drawing (SMD): [5962-15228](#)

SEE Test Objectives

The ISL72027SEH was tested to determine its susceptibility to destructive single event effects (collectively referred to as SEB) and to characterize its Single Event Transient (SET) behavior over various operating conditions. Since the family of parts utilizes the same silicon with only bond-out options, it was determined that testing the ISL72027SEH would serve to characterize all three parts. More description of the part differences follows in the next two paragraphs. Thereafter the report will refer only to the ISL72027SEH with the understanding that the results apply equally to the other two members of the family, the ISL72026SEH and ISL72028SEH.

The ISL72026SEH and ISL72027SEH differ in that the Loopback (LBK) command input of the ISL72026SEH is not bonded out in the ISL72027SEH. Instead, V_{REF} is bonded out in the ISL72027SEH. All other pins and functions are the same. Since the LBK has an internal pull-down, the LBK function is constantly deasserted in the ISL72027SEH, but the LBK circuitry is fully active and available to SEE events that

could cause LBK to be momentarily asserted. On the other hand, the V_{REF} circuitry is fully active in the ISL72026SEH, however, is simply not brought out to the outside world. Consequently, all that is lost in testing the ISL72027SEH rather than the ISL72026SEH is that the part is not tested while in the LBK mode. Since this is a diagnostic mode and is expected to be active only a very small fraction of the operational life, it does not seem to represent a statistically important mode for SEE events. The jeopardy is that an SET could momentarily take the part out of LBK, however, this would be an extremely unlikely event if LBK is not a dominant operational mode.

The ISL72028SEH differs from the ISL72027SEH in that the RS pin when pulled to VCC can invoke a Low Power Shutdown (LPSD) mode rather than the Listen Mode (LM) of the ISL72027SEH. Both circuits are operational in both parts; it is just that a pin control is only effective according to the part type. So, if either the LM or LPSD can be activated by SEE, either circuit would be susceptible. What is lost in testing the ISL72027SEH is the event where an SET triggers the ISL72028SEH out of LPSD. Such an event would be of little interest to the operation of the system so it is not perceived as an important omission.

SEE Test Facility

Testing was performed at the Texas A&M University (TAMU) Radiation Effects Facility of the Cyclotron Institute heavy ion facility. This facility is coupled to a K500 superconducting cyclotron, which is capable of generating a wide range of particle beams with the various energy, flux and fluence levels needed for advanced radiation testing. The Devices Under Test (DUTs) were located in air at 40mm from the aramica window for the ion beam. The ion LET values are quoted at the DUT surface. Signals were communicated to and from the DUT test fixture through 20 foot cables connecting to the control room. Testing was carried out over four trips to TAMU, on November 7th and 8th of 2014, December 1st of 2014, March 18th of 2015 and June 2nd of 2015.

SEE Test Set-Up

SEE testing was carried out with the samples in an active configuration. The schematic of the ISL72027SEH SEE test fixture used in 2015 is shown in [Figure 1](#). This schematic shows direct access to the CANH/CANL bus pins for monitoring and indirect access through 30 Ω resistors for biasing. These resistor feeds were not there in the 2014 testing so that bus bias and monitor were done through the same lines. The cabling connected to the CANH/CANL pins present 700pF to GND due to the 20 foot cable connecting the DUT to the oscilloscopes in the control room for SET testing. Other supplies and signals indicated by arrows were also cabled to the control room.

March 2015 SEB Testing of the ISL72027SEH CAN Transceiver

Four units of the ISL72027SEH were irradiated for the purposes of destructive SEE (SEB) testing. Four currents and the V_{REF} output voltage were monitored as in [Table 1 on page 4](#) to determine if permanent change was induced during irradiations. After initial measurements according to [Table 1](#), a set of six irradiations was performed as listed in [Table 2 on page 4](#). Each irradiation was done with 2.114GeV Pr (praseodymium) at 10° incidence for a surface LET = $60\text{MeV} \cdot \text{cm}^2/\text{mg}$ to a fluence of 5×10^6 ion/cm² per irradiation at fluxes under 2.5×10^4 ion/(cm²*s). The ICC and ICM were measured before and after each irradiation to look for indications of damage in changes of those parameters. At the end of the set of six irradiations the parameters in [Table 1](#) were again measured to look for any changes.

The 50kHz data signal allowed for the common-mode voltage to dominate the bus pins during the recessive periods but still exercised switching conditions. [Figures 2](#) and [3](#) offer examples of the timing requiring the 50kHz input signal. The 47nF capacitor on V_{REF} and the resistors in the V_{CM} path were what set the time constant of the common-mode voltage. The complement of six irradiations accounted for 58krad of total dose when combined

with a similar set done with common-mode voltages of $\pm 17\text{V}$ before moving on to the $\pm 18\text{V}$ set reported here. The device case temperature was heated to $+125^\circ\text{C} \pm 10^\circ\text{C}$ for the irradiations with a thin film heater mounted on the board. The heater setting was calibrated with a thermocouple on the case at the Intersil lab before traveling to TAMU. At TAMU the heater was set to the predetermined setting to yield the $+125^\circ\text{C}$ case temperature. At the end of the six irradiations outlined in [Table 2](#) the monitor parameter measurements of [Table 1](#) were repeated to check for changes.

[Table 3](#) presents the log of the ICC and ICM measurements made for each irradiation run at the conditions described in [Table 2](#). The same data is presented in [Table 4 on page 5](#) as the percentage change in the measured currents. Changes of less than 5% were considered to be within measurement error and not interpreted as indicative of damage. [Table 5 on page 5](#) presents the measurements of monitor parameters in [Table 1](#) made both before and after the groupings of six irradiations. [Table 6 on page 5](#) presents the monitor data of [Table 5](#) as percentage change. Again changes of 5% or less are viewed as within measurement error. On the basis of these tests the part is found to be free of damaging SEE up to LET = $60\text{MeV} \cdot \text{cm}^2/\text{mg}$ (Pr at 10° incidence) and the conditions listed in [Table 2](#).

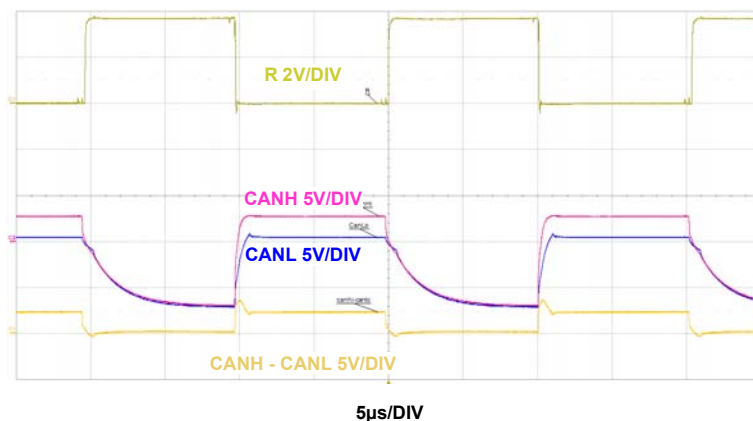


FIGURE 2. Example of CANH/CANL switching at 50kHz, $V_{CC} = 3.6\text{V}$ and a common-mode of -7V . Time allows recessive state to stabilize at -7V for the CANH/CANL lines. Time scale is $5\mu\text{s}/\text{div}$, and the vertical axis is $2\text{V}/\text{div}$ for the upper plot and $5\text{V}/\text{div}$ for the lower three plots.

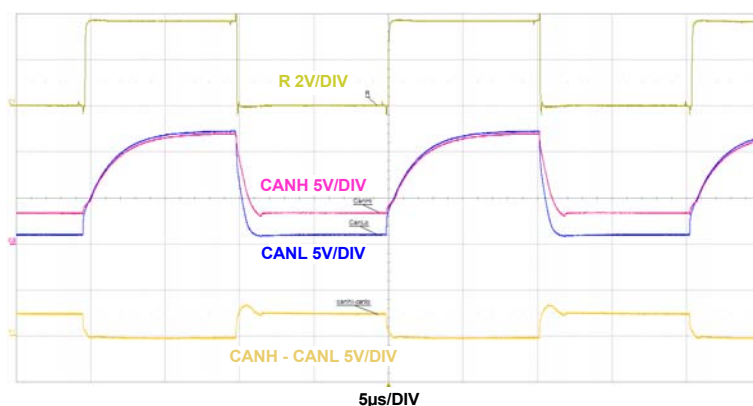


FIGURE 3. Example of CANH/CANL switching at 50kHz, $V_{CC} = 3.6\text{V}$, and a common-mode of $+12\text{V}$. Time allows recessive state to stabilize at $+12\text{V}$ for the CANH/CANL lines. Time scale is $5\mu\text{s}/\text{div}$, and the vertical axis is $2\text{V}/\text{div}$ for the upper plot and $5\text{V}/\text{div}$ for the lower three plots.

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TABLE 1. MONITOR MEASUREMENTS AND CONDITIONS FOR SEB DETECTION

MEASUREMENTS MADE	ELECTRICAL CONDITIONS FOR MEASUREMENT									
	RS (V)	D	VCC (V)	VR (V)	K1	K2	V _{CM} (V)	CANH	CANL	R
ICM (μA) at V _{CM} = -7V	0	4.5	3.6	OP	CL	OP	-7	CH2	CH3	OP
ICM (μA) at V _{CM} = +12V	0	4.5	3.6	OP	CL	OP	+12	CH2	CH3	OP
VREF at V _{CM} (V)	0	4.5	3.6	OP	OP	CL	Meas. V _{REF}	CH2	CH3	OP
ICC (mA) Dynamic Unloaded	0	0V to 4.5V 250kHz	3.6	OP	OP	OP	OP	CH2	CH3	OP
ICC (mA) Dynamic Loaded Slow	OP	0V to 4.5V 250kHz	3.6	1.7V	CL	CL	OP	CH2	CH3	OP
Scope Capture Loaded Slow, 2μs/div	OP	0V to 4.5V 250kHz, CH1	3.6	1.7V	CL	CL	OP	CH2	CH3	CH4

NOTE: OP = Open and CL = Closed. Measurements of these parameters were made at the start and end of the six SEB tests listed in [Table 2](#). Oscilloscope channels are indicate by "CH".

TABLE 2. SEB TESTS RUN ON ISL72027 DURING THE MARCH 2015 TESTING

	RS (V)	D	VCC (V)	K1	K2	V _{CM} (V)
Cold Spare -18V _{CM}	0	0V to 4.5V 50kHz	0	CL	CL	-18
Cold Spare +18V _{CM}	0	0V to 4.5V 50kHz	0	CL	CL	+18
Fast Op -18V _{CM}	0	0V to 4.5V 50kHz	4.5	CL	OP	-18
Fast Op +18V _{CM}	0	0V to 4.5V 50kHz	4.5	CL	OP	+18
Slow Op -18V _{CM}	OP	0V to 4.5V 50kHz	4.5	CL	CL	-18
Slow Op +18V _{CM}	OP	0V to 4.5V 50kHz	4.5	CL	CL	+18

TABLE 3. SUPPLY CURRENT MONITORS ICC AND ICM FOR EACH IRRADIATION WITH Pr AT 10° FOR LET of 60MeV • cm²/mg TO 5x10⁶ Ion/cm² FOR EACH IRRADIATION.

IRRADIATION CONDITION V _{CC} = 4.5V		DUT1		DUT2		DUT3		DUT4	
		ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)
Cold Spare V _{CM} = -18V	Pre		0.0076		0.0075		0.0075		0.0075
	Post		0.0075		0.0073		0.0075		0.0075
Cold Spare V _{CM} = +18V	Pre		0.0075		0.0077		0.0075		0.0075
	Post		0.0075		0.0076		0.0074		0.0075
Fast Op V _{CM} = +18VN	Pre	3.24	7.85	3.67	8.39	3.26	8.16	3.7	7.48
	Post	3.25	7.83	3.65	8.40	3.246	8.22	3.69	7.49
Fast Op V _{CM} = -18V	Pre	13.01	9.26	14.53	10.37	14.17	10.43	13.26	9.10
	Post	13.16	9.31	14.53	10.39	14.14	10.39	13.27	9.11
Slow Op V _{CM} = -18V	Pre	8.08	4.88	8.61	5.00	8.39	5.21	8.72	5.05
	Post	8.08	4.89	8.61	5.01	8.4	5.22	8.72	5.05
Slow Op V _{CM} = +18V	Pre	3.36	51.07	3.71	52.35	3.48	52.60	3.76	54.00
	Post	3.33	51.80	3.72	52.5	3.38	52.09	3.74	53.53

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TABLE 4. SUPPLY CURRENT MONITOR DELTAS (ICC AND ICM) FOR EACH IRRADIATION WITH Pr AT 10° FOR LET OF 60MeV • cm²/mg TO 5x10⁶ion/cm² FOR EACH IRRADIATION.

IRRADIATION CONDITION V _{CC} = 4.5V	DUT1		DUT2		DUT3		DUT4	
	ICC DELTA%	ICM DELTA%	ICC DELTA%	ICM DELTA%	ICC DELTA%	ICM DELTA%	ICC DELTA%	ICM DELTA%
Cold Spare -18V _{CM}		-1		-3		0		0
Cold Spare +18V _{CM}		0		-1		-1		0
Fast Op +18V _{CM}	0	0	-1	0	0	1	0	0
Fast Op -18V _{CM}	1	1	0	0	0	0	0	0
Slow Op -18V _{CM}	0	0	0	0	0	0	0	0
Slow Op +18V _{CM}	-1	1	0	0	-3	-1	-1	-1

TABLE 5. PARAMETRIC MONITORS FOR EACH SET OF IRRADIATIONS

		ICM (μA) AT V _{CM} = -7V	ICM (μA) AT V _{CM} = +12V	V _{REF} AT V _{CM} (V)	ICC (mA) UNLOADED FAST	ICC (mA) LOADED SLOW
DUT1	Pre	608	652	1.773	4.11	24.10
	Post	604	649	1.772	4.10	24.05
DUT2	Pre	604	652	1.769	4.51	24.38
	Post	600	649	1.768	4.51	24.45
DUT3	Pre	598	645	1.773	4.11	24.90
	Post	600	644	1.775	4.12	25.14
DUT4	Pre	609	657	1.772	4.55	25.05
	Post	611	656	1.774	4.54	25.11

NOTE: Refer to [Table 2 on page 4](#). Irradiation was with Pr at 10° incidence for effective let of 60MeV • cm²/mg and each set of irradiations having a total of 3x10⁷ion/cm².

TABLE 6. DELTAS OF PARAMETRIC MONITORS FOR EACH SET OF IRRADIATIONS

	ICM (μA) AT V _{CM} = -7V (%)	ICM (μA) AT V _{CM} = +12V (%)	V _{REF} AT V _{CM} (V%)	ICC (mA) UNLOADED FAST (%)	ICC (mA) LOADED SLOW (%)
DUT1	-1	0	0	0	0
DUT2	-1	0	0	0	0
DUT3	0	0	0	0	1
DUT4	0	0	0	0	0

NOTE: Refer to [Table 2 on page 4](#). Irradiation was with Pr at 10° incidence for effective let of 60MeV • cm²/mg and each set of irradiations having 3x10⁷ion/cm².

[Tables 5](#) and [6](#) present the collected data for the parameters of [Table 1](#) across the irradiation sets. Again no change was noted that indicated permanent damage to the parts.

It was deduced from the above testing that the ISL72027SEH was found to be free from destructive SEE effects from ions with effective LET of 60MeV • cm²/mg while biased at V_{CC} = 4.5V and V_{CM} = ±18V.

SET Testing of the ISL72027SEH CAN Transceiver at Ag (LET = 43MeV • cm²/mg)

Testing for Single Event Transients (SET) was carried out using silver (Ag) at 1.634GeV for a surface LET = 43MeV • cm²/mg. Beam time constraints on the trip limited the testing to only two units. A summary of the conditions tested and the SET counts resulting appear in [Table 7](#). Examples of the SET captured in the irradiation runs appear in [Figures 4](#) through [7](#).

There were stand-alone errant recessive bits of approximately 2μs duration at 43MeV • cm²/mg as well as spike recessive events seen in [Figure 4](#). These occurred for the bus VOD biased externally at the receiver dominant threshold of 0.9V.

The events in [Figure 5](#) are errant dominant spikes occurring on the R output, either with or without concomitant disruption on the VOD signal. In these cases, the bus VOD was externally biased to 0.5V, the receiver recessive threshold. When disturbances on VOD were noted, the erroneous dominant spikes generally came in pairs as on the left side to [Figure 5](#), following the ringing on VOD.

The dynamic testing was done by providing a square wave input to the D pin (0V to 3V) and monitoring the response of the receiver R pin signal. When the transceiver was set to the slow slew rating of the transmitter, a frequency of 250kHz was used. When the transceiver was set for fast slewing of the transmitter a 500kHz signal was used, except in the two inadvertent cases of lines eleven and twelve of [Table 7](#).

[Figures 6](#) and [7](#) present examples of the worst dynamic SET that were captured using silver.

The two events represented in the top of [Figure 6](#) have clear disturbances on VOD associated with the disruption of the bit stream on R. As with the static tests, these appear to be transmitter SET that are simply reflected in the receiver output. The bottom event in [Figure 6](#) is not clearly associated with a VOD disturbance, however, it certainly occurs during a VOD transition and at the received bit edge. Again a transmitter SET seems to be indicated.

For the high speed events in [Figure 7](#), each SET on R is accompanied by what appears to be a precipitating SET on the VOD signal. Thus, these are all consistent with transmitter events and not receiver SET.

TABLE 7. STATIC CAPTURES AND DYNAMIC SET CAPTURES

TEST CONDITIONS	DUT1 EVENTS	DUT2 EVENTS	DUT2 TOTAL EVENTS	NET CROSS SECTION (cm ²)
VOD Dominant V _{THR} 0.9V	18	14	32	8.0x10 ⁻⁶
VOD Recessive V _{THF} 0.5V	42	51	93	2.3x10 ⁻⁵
Listen only, VOD Dominant V _{THR} 1.05V	0	0	0	-
Listen only, VOD Recessive V _{THF} 0.65V	0	0	0	-
Transmit Slow 250kHz Open CM and V _{REF}	9	14	23	5.8x10 ⁻⁶
Transmit Slow 250kHz Open CM	13	15	28	7.0x10 ⁻⁶
Transmit Slow 250kHz -7V _{CM} and V _{REF}	21	16	37	9.3x10 ⁻⁶
Transmit Slow 250kHz -7V _{CM}	17	15	32	8.0x10 ⁻⁶
Transmit Slow 250kHz +12V _{CM} and V _{REF}	10	6	16	4.0x10 ⁻⁶
Transmit Slow 250kHz +12V _{CM}	5	4	9	2.3x10 ⁻⁶
Transmit Slow 500kHz Open CM and V _{REF}	83	87	170	4.3x10 ⁻⁵
Transmit Slow 500kHz Open CM	95	76	171	4.3x10 ⁻⁵
Transmit Fast 500kHz -7V _{CM} and V _{REF}	12	4	16	4.0x10 ⁻⁶
Transmit Fast 500kHz -7V _{CM}	2	7	9	2.3x10 ⁻⁶
Transmit Fast 500kHz +12V _{CM} and V _{REF}	2	2	4	1.0x10 ⁻⁶
Transmit Fast 500kHz +12V _{CM}	1	4	5	1.3x10 ⁻⁶

NOTE: Static captures were for any change of R state, while dynamic captures were taken for R duty cycle outside of 40% to 60%. The irradiations were with Ag at normal incidence for an LET = 43MeV • cm²/mg and the device at ambient temperature (~25°C). A fluence of 2x10⁶ions/cm² was done for each irradiation.

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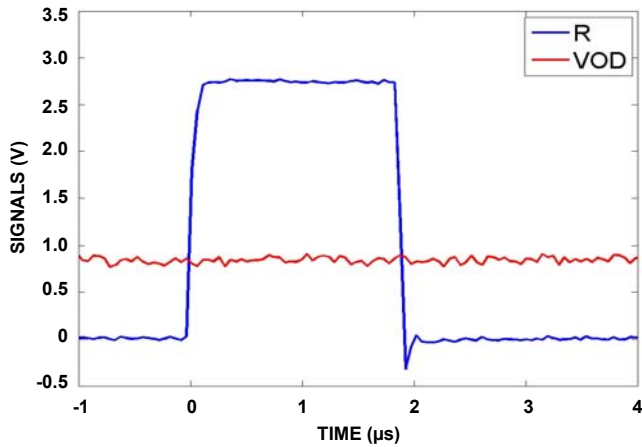


FIGURE 4A.

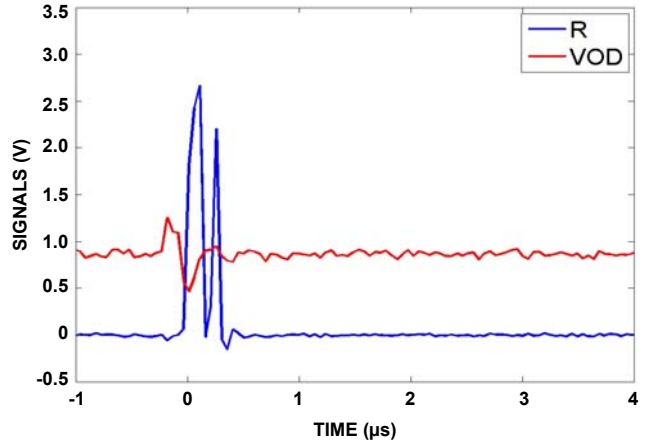


FIGURE 4B.

FIGURE 4. The left hand SET (Figure 4A) goes from dominant to recessive with no apparent SET on VOD (5/32 in 4×10^6 fluence). The case on the right (Figure 4B) shows recessive spikes along with a disturbance on VOD and accounted for 27/32 events captured in 4×10^6 fluence.

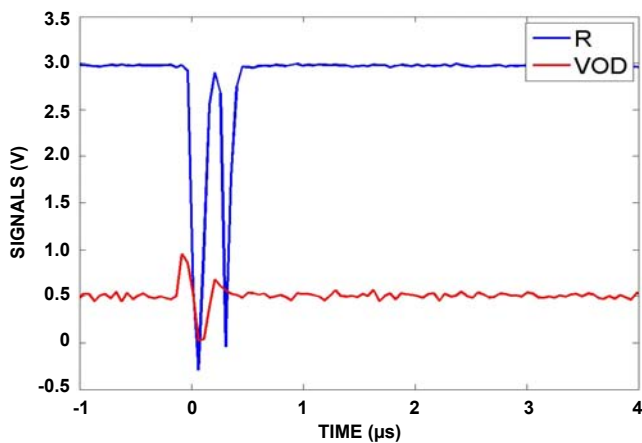


FIGURE 5A.

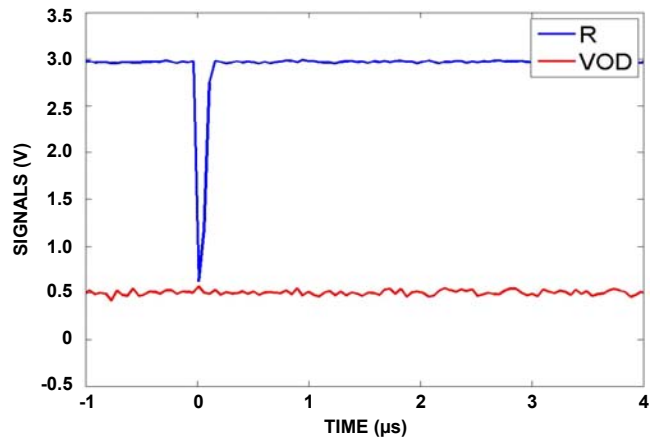


FIGURE 5B.

FIGURE 5. The left hand SET (Figure 5A) shows dominant spikes in R along with an SET on VOD (17/93). In the right hand (Figure 5B) case a single dominant spike is unaccompanied by and discernable VOD SET (76/93). The fluence is 4×10^6 .

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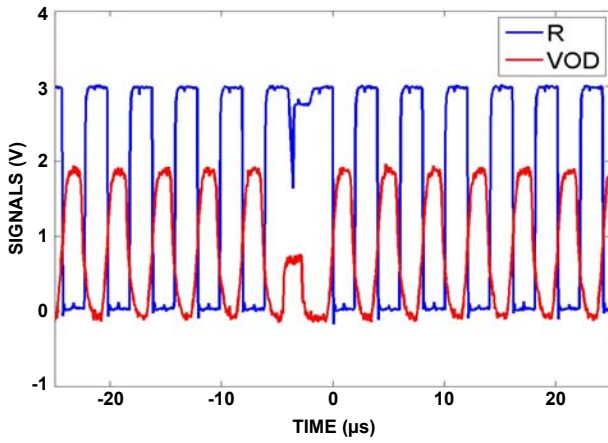


FIGURE 6A. TRANSMIT SLOW OPEN CM

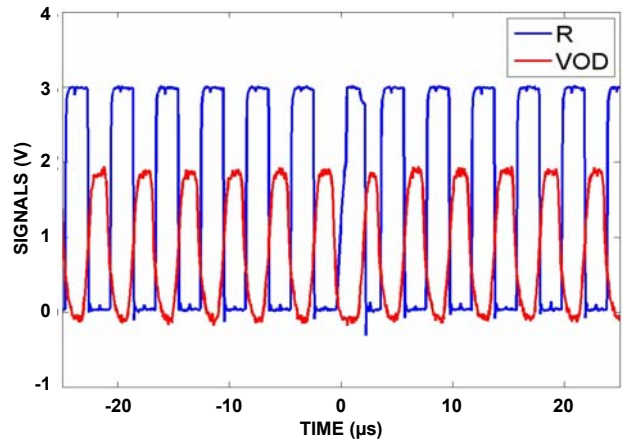


FIGURE 6B. TRANSMIT SLOW OPEN CM AND V_{REF}

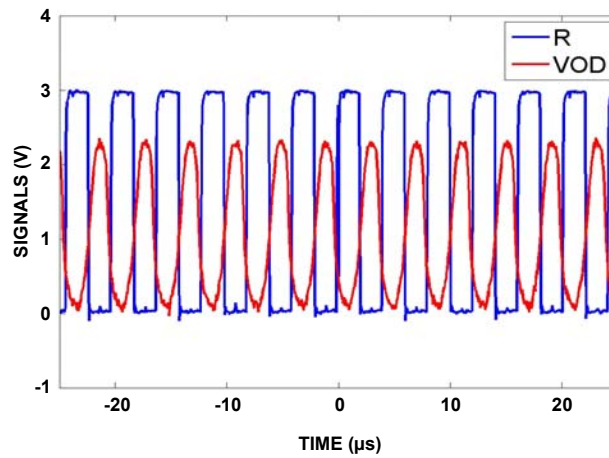


FIGURE 6C. TRANSMIT SLOW $-7V_{CM}$ AND V_{REF}

FIGURE 6. The longest recessive event is in the upper left (Transmit Slow Open CM) and the longest dominant event is the upper right (transmit slow open CM and V_{REF}). The bottom capture shows a glitch at the leading edge of a recessive bit (transmit slow $-7V_{CM}$ and V_{REF}).

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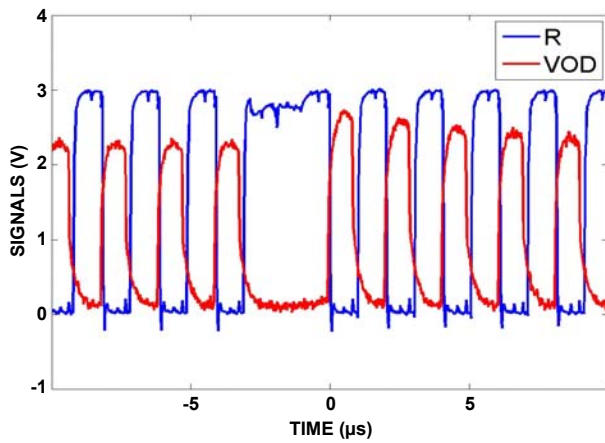


FIGURE 7A. TRANSMIT FAST $-7V_{CM}$ AND V_{REF}

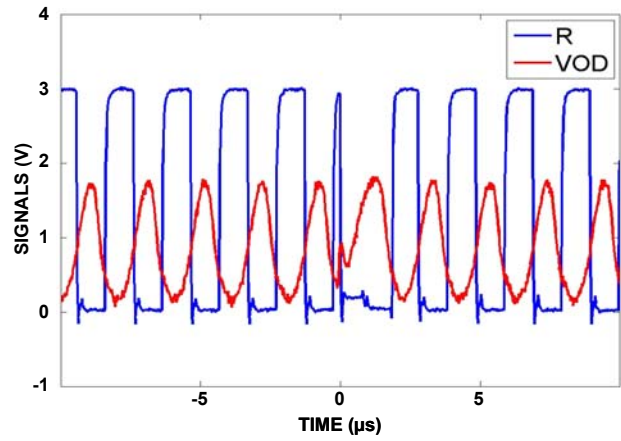


FIGURE 7B. TRANSMIT FAST OPEN CM

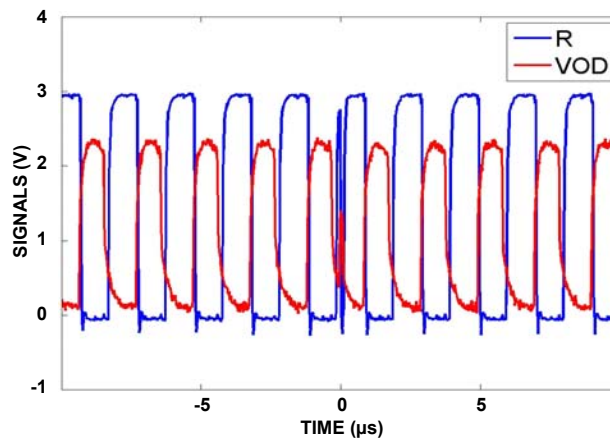


FIGURE 7C. TRANSMIT FAST $-7V_{CM}$ AND V_{REF}

FIGURE 7. The upper left (Figure 7A) shows the longest recessive time (Transmit Fast $-7V_{CM}$ and V_{REF}), the upper right (Figure 7B) the longest dominant time (transmit fast open CM). The lower capture (Figure 7C) shows a dominant spike during a recessive bit (transmit fast $-7V_{CM}$ and V_{REF}). The plot at upper right (Figure 7B) indicates that the transition speed was not actually set to the high speed setting.

SET Testing of the ISL72027SEH CAN Transceiver at Cu (LET = 20MeV • cm²/mg)

Since SET occurred for LET = 43MeV • cm²/mg tests were run at the lower LET = 20MeV • cm²/mg using copper. The biasing conditions run were restricted to exclude common-mode biasing cases since in the higher LET testing the common-mode conditions did not substantially influence the SET observations. The tests run and the event counts appear in [Table 8](#) while examples of the worst SET observed follow in [Figures 8](#) through [10](#).

In the case of [Figure 8](#), the SETs on R are all associated with preceding disturbances on VOD that indicate an SET to the transmitter that impacts the VOD. In these cases, the SET on R is a response to a transmitter SET and not a receiver SET. The ringing on VOD is certainly the result of the cabling used to monitor the VOD voltage. In total, the cross section of these events on four parts is approximately 3.22x10⁻⁶cm²

[Figure 9](#) looks at dominant SET occurring when the bus is biased at the recessive threshold of 0.5V. In this case, two distinct types of SET seem to occur. The first is a double spike with a preceding disturbance on the bus (VOD). This would appear to be a transmitter SET that is simply reflected in the receiver output. The second case is a single dominant spike that does not appear to be associated with any real disturbance on the bus (VOD). This would appear to be a genuine receiver SET. Both types of events disappear when the bus is left open rather than being biased to the recessive threshold value.

[Figure 10](#) looks at the worst SET occurring with a dynamic bit stream being transmitted with no common-mode. The first two plots are for a 250kHz input signal (500kbit/s alternating 1's and 0's) with slow bus transitions while the third plot is for 500kHz with fast transitions selected. The only events recorded on R were dominant glitches associated with the edges of the bits when the bus (VOD) was in a transition. The SET were all associated with distortions on the VOD waveform and so are believed to originate in the transmitter.

TABLE 8. SET TESTING AT LET = 20MeV • cm²/mg AND FLUENCE OF 1x10⁷Ion/cm² FOR EACH RUN

TEST CONDITIONS	DUT1 EVENTS	DUT2 EVENTS	DUT3 EVENTS	DUT4 EVENTS	CROSS SECTION (cm ²)
VOD Dominant at 1V	20	32	38	39	3.2x10 ⁻⁶
VOD Dominant V _{THR} 0.9V	38	45			4.2x10 ⁻⁶
VOD Recessive V _{THF} 0.5V	65	47	71	78	6.5x10 ⁻⁶
Transmit Dominant Open CM	0	0			–
Transmit Recessive Open CM	0	0			–
Transmit Slow (250kHz) Open CM	13	10	3	9	8.8x10 ⁻⁷
Transmit Fast (500kHz) Open CM	362*	85*	3	4	3.5x10 ⁻⁷

NOTE: The runs marked with an asterisk (*) were accidentally run at slow transition speeds but at higher data rate; this accounts for the higher event counts.

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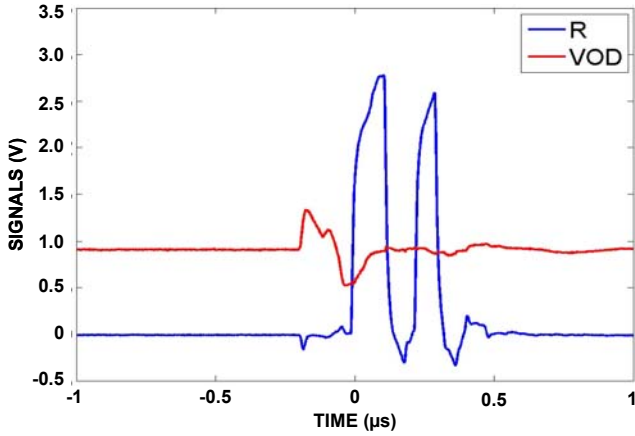


FIGURE 8A.

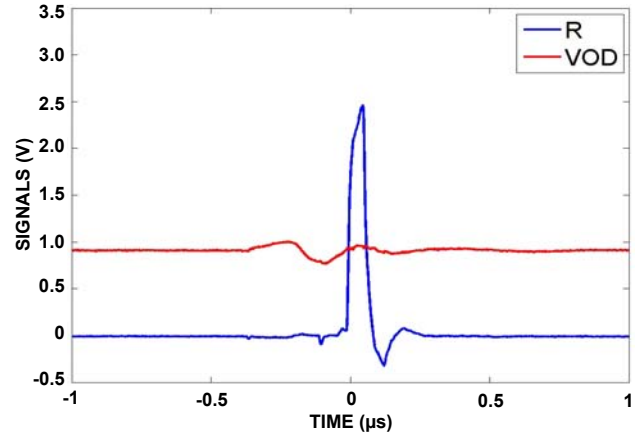


FIGURE 8B.

FIGURE 8. Examples of dominant to recessive SET for a dominant threshold (0.9V) on the bus. For DUT1 the double spikes on the left plot (Figure 8A) represented 21/38 events; the single spikes on the right (Figure 8B) represented the other 17/38 events. The total fluence at LET = 20MeV • cm²/mg was 1x10⁷ion/cm². For all events the SET on VOD preceded the SET on R.

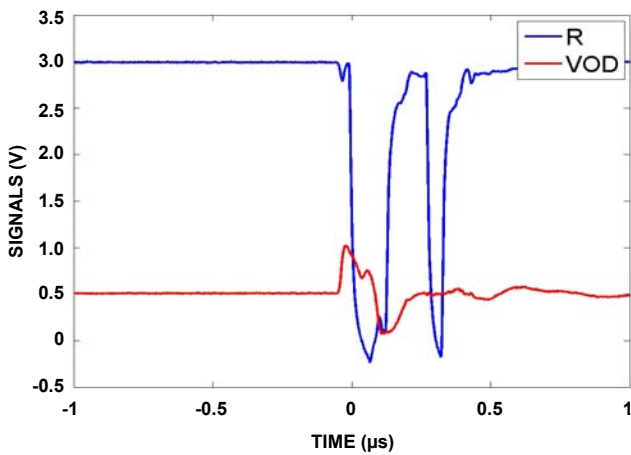


FIGURE 9A.

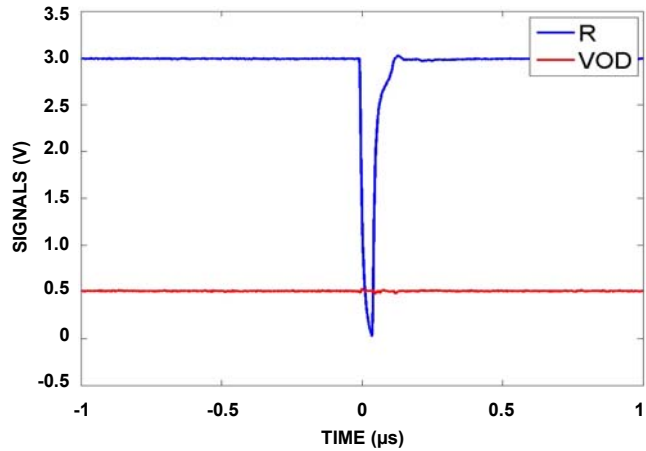


FIGURE 9B.

FIGURE 9. Examples of recessive to dominant SET from DUT1 for recessive threshold (0.5V) on the bus. The double spikes on the left plot (Figure 9A) represented 21/65 events; the single spikes on the right (Figure 9B) represented the other 44/65 events. The total fluence per run at LET = 20MeV • cm²/mg was 1x10⁷cm². Only the double spikes on the left showed clear VOD SET preceding the R SET. The single spikes appear not to have an associated VOD event.

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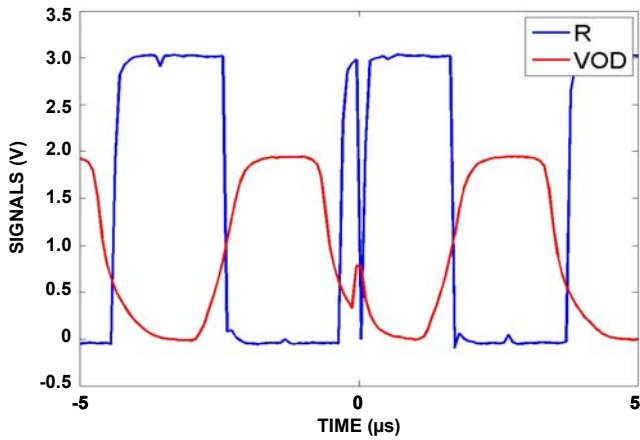


FIGURE 10A.

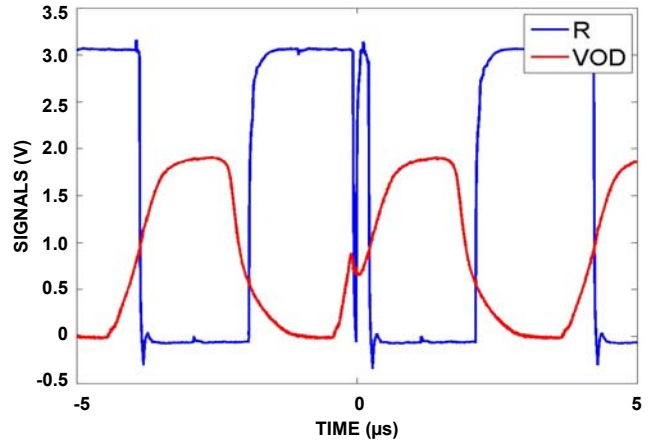


FIGURE 10B.

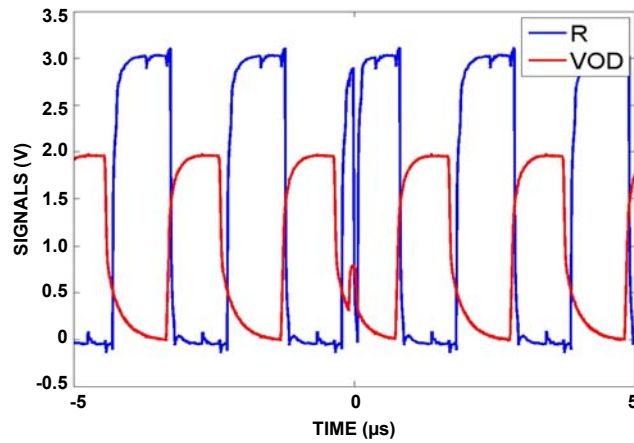


FIGURE 10C.

FIGURE 10. Examples of SET during data transmission. The top events (Figures 10A and 10B) are for slow transmission (DUT1 and DUT2) and the bottom (Figure 10C) is fast transmission (DUT3). The SET exhibit VOD transients during transition that result in false dominant SET on the R output. The total fluence per run at LET = $20\text{MeV} \cdot \text{cm}^2/\text{mg}$ was $1 \times 10^7 \text{cm}^2$. The top plots (Figures 10A and 10B) indicate that SET can occur on either transition of the VOD. Unlike results at LET = $43\text{MeV} \cdot \text{cm}^2/\text{mg}$ there were no missing bits of either state.

SET Testing of the ISL72027SEH CAN Transceiver at LET = 8.5 and 2.7MeV • cm²/mg

SET testing was again done on the ISL72027SEH with Ar (LET = 8.5MeV • cm²/mg) and Ne (LET = 2.7MeV • cm²/mg). With argon, events were only recorded for the case of the bus operating at the dominant threshold of 0.9 V and for dynamic operation as represented in [Table 9](#). With neon, (2.7MeV • cm²/mg) no SET at all were observed. Again beam time constraints limited only two units being tested.

For the static SET observed with VOD = 0.9V (dominant threshold), there were observed recessive spikes, either single or double spikes, as depicted in [Figure 11](#). Twenty five of the fifty-eight SET observed were of the double spike variety. All the observed SET began with what appears to be an attempt of the transmitter to assert a dominant state on the CAN bus (rise in VOD) followed by some ringing on the bus that was interpreted by the receiver as being a recessive state. This is consistent with no SET being observed for an applied VOD of 1.5V, where the errant

dominant state would not cause a transient sufficient to result in bus ringing to invoke a recessive state on the receiver.

The dynamic SET were almost non-existent with only four being recorded for the fast slew setting. All four look quite similar and are represented in the top two plots of [Figure 12](#). In the first plot [Figure 12A](#) no apparent disturbance can be discerned in the VOD trace, while in the second plot [Figure 12B](#) a clear glitch in the VOD trace is evident. In both cases the R transition from dominant to recessive is interrupted by a spike back to dominant. The spikes occur during the transition and are on the order of 100ns in duration. The third SET (bottom of [Figure 12C](#)) shows a clear VOD glitch on the slower slew rate transition of the VOD signal.

TABLE 9. RESULTS FOR SET TESTING WITH LET = 8.5MeV • cm²/mg (Ar) TO 1x10⁷ Ion/cm² PER RUN

TEST CONDITIONS	DUT1 EVENTS	DUT2 EVENTS	TOTAL EVENTS	CROSS SECTION (cm ²)
Recessive Xmit Open Bus, High Slew	0	0	0	-
Recessive Xmit Open Bus, Medium Slew	0	0	0	-
Dominant Xmit Open Bus, High Slew	0	0	0	-
Dominant Xmit Open Bus, Medium Slew	0	0	0	-
VCANH = 1.9V, VCANL = 1.0V, High Slew	29	29	58	2.9x10 ⁻⁶
VCANH = 1.9V, VCANL = 1.0V, Medium Slew	31	31	62	3.1x10 ⁻⁶
VCANH = 2.5V, VCANL = 1.0V, High Slew	0	0	0	-
VCANH = 2.5V, VCANL = 1.0V, Medium Slew	0	0	0	-
Transmit 500kHz, Fast, No CM or V _{REF}	4	0	4	2x10 ⁻⁷
Transmit 500kHz, Medium, No CM or V _{REF}	1	0	1	5x10 ⁻⁸

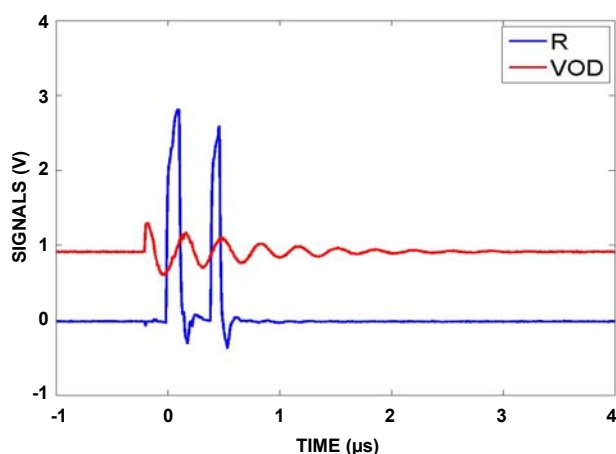


FIGURE 11A.

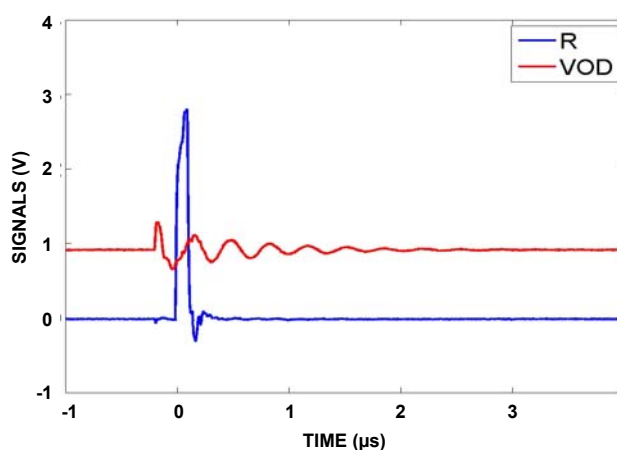


FIGURE 11B.

FIGURE 11. Example SET for LET = 8.5MeV • cm²/mg with VCANH = 1.9V AND VCANL = 1V (V_{OD} = 1.5V).

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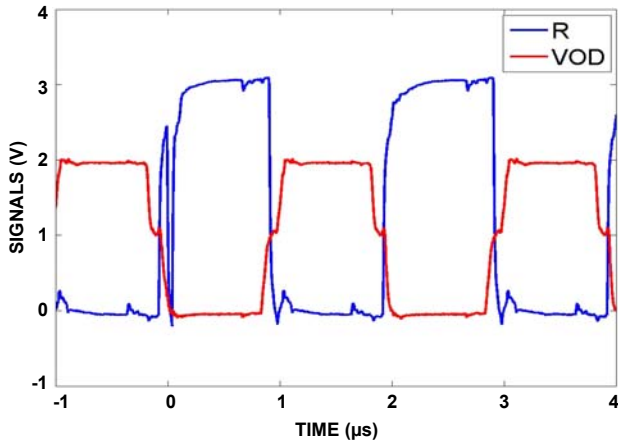


FIGURE 12A.

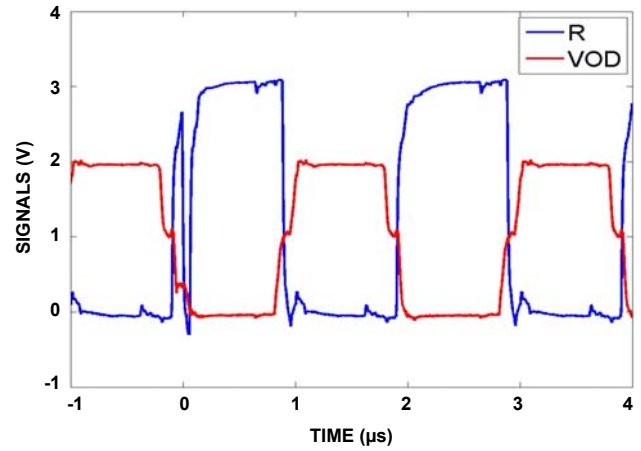


FIGURE 12B.

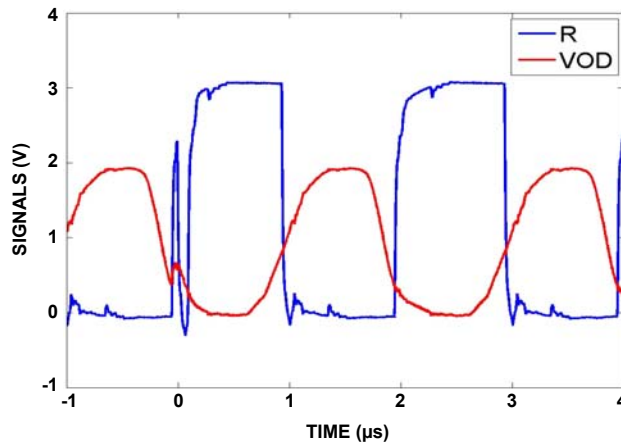


FIGURE 12C.

FIGURE 12. Examples of dynamic SET at LET = 8.5MeV • cm²/mg for fast slew (Figures 12A and 12B) and for medium slew (Figure 12C).

Discussion and Conclusions

Damaging SEE

Testing of the ISL72027SEH at case temperatures of $+125^{\circ}\text{C} \pm 10^{\circ}\text{C}$ and $60\text{MeV} \cdot \text{cm}^2/\text{mg}$ did not yield damaging SEE effects with a supply of $V_{\text{CC}} = 4.5\text{V}$ and the CAN bus common-mode (CANH, CANL) at $\pm 18\text{V}$. The tests were run on four parts to 5×10^6 ions/ cm^2 on each of six irradiation runs per part including both polarities of common-mode for cold sparing, and for fast and slow transmitter slewing. Consequently it is concluded that the part is immune to damaging SEE effects at $60\text{MeV} \cdot \text{cm}^2/\text{mg}$ while operating at or below the voltages of $V_{\text{CC}} = 4.5\text{V}$ and bus common-mode voltages of $\pm 18\text{V}$.

Single Event Transients

The ISL72027SEH exhibited SET susceptibility at $\text{LET} = 43, 20$ and $8.5\text{MeV} \cdot \text{cm}^2/\text{mg}$. SET was defined as any transition in the receiver output for static biasing conditions and any received bit outside of 40% to 60% duty-cycle for a 50% transmitted bit stream. No SET of either type were recorded at an $\text{LET} = 2.7\text{MeV} \cdot \text{cm}^2/\text{mg}$.

At the higher LET level ($43\text{MeV} \cdot \text{cm}^2/\text{mg}$), SET represented by [Figure 4A](#) were noted. The receiver dominant signal was interrupted for nearly $2\mu\text{s}$ by an errant recessive received signal while the bus was being externally biased to 0.9V . This type of SET represented a cross-section at $43\text{MeV} \cdot \text{cm}^2/\text{mg}$ of approximately $1.3 \times 10^{-6}\text{cm}^2$. This type of event disappeared at $\text{LET} = 20\text{MeV} \cdot \text{cm}^2/\text{mg}$ and below.

The form of SET depicted in [Figure 4B](#), a recessive receiver spike or double spike during a dominant bus voltage of 0.9V , occurred for LET down to $8.5\text{MeV} \cdot \text{cm}^2/\text{mg}$ with a cross-section down to $3.0 \times 10^{-6}\text{cm}^2$ at that LET. These events disappeared at $\text{LET} = 2.7\text{MeV} \cdot \text{cm}^2/\text{mg}$ to yield a cross-section limit of $5 \times 10^{-8}\text{cm}^2$.

With the bus externally biased to the recessive threshold of 0.5V , SET consisting of receiver dominant spikes as in [Figure 5](#) were noted. Most of these SET correlated to VOD disturbances indicating a transmitter SET as the initiating event, though some of the shortest events were not accompanied by a VOD disturbance. At an LET of $20\text{MeV} \cdot \text{cm}^2/\text{mg}$ these events had a cross-section of $6.5 \times 10^{-6}\text{cm}^2$.

Dynamic testing of the part for SET resulted in missing bits at the receiver as in [Figures 6](#) and [7](#) for $43\text{MeV} \cdot \text{cm}^2/\text{mg}$. At LET of $20\text{MeV} \cdot \text{cm}^2/\text{mg}$ and below dynamic testing only resulted in glitches on the transitions of the bits as in [Figures 10](#) and [12](#). At LET of $8.5\text{MeV} \cdot \text{cm}^2/\text{mg}$ the cross-section for these SET was $2.0 \times 10^{-7}\text{cm}^2$. At LET of $2.7\text{MeV} \cdot \text{cm}^2/\text{mg}$ there were no SET recorded to a nominal $5 \times 10^{-8}\text{cm}^2$.

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TABLE 10. SEB TESTS RUN ON ISL72027 DURING THE SEPTEMBER 2015 TESTING

	RS (V)	D	VCC (V)	K1	K2	VCM (V)
Cold Spare -20V _{CM}	0	0V to 5.5V 50kHz	0	CL	CL	-20
Cold Spare +20V _{CM}	0	0V to 5.5V 50kHz	0	CL	CL	+20
Slow Op -20V _{CM}	OP	0V to 5.5V 50kHz	5.5	CL	CL	-20
Slow Op +20V _{CM}	OP	0V to 5.5V 50kHz	5.5	CL	CL	+20

September 2015 Addendum

Subsequent to the previous report, further testing for damaging SEE (referred to as SEB but to include SEL and SEGR) was done on the ISL72027SEH parts on September 26th of 2015. Two major changes were introduced into the testing. First the testing was done at +25°C ambient rather than +125°C case temperature. Second, the voltages used for testing were increased to ±20V for the common-mode voltage to the bus pins and +5.5V on the supply pin VCC when powered.

The ion species used was again Praseodymium (Pr) with the in-air path lengthened to yield a surface LET of 60MeV • cm²/mg at a 0° angle of incidence. Each irradiation was taken to a fluence of 1x10⁷ ion/cm². Four tests were run on each of four units as described in [Table 10](#).

As done previously, the supply current (ICC) and the bus common-mode current (ICM) were monitored before and after each irradiation and are reported in [Table 11](#). The deltas for ICC and ICM are presented in [Table 12](#). The changes in ICC and ICM do not provide any indication of damage due to the irradiations.

Before and after each grouping of the four tests indicated in [Table 10](#), the monitor parameters as described in [Table 1](#) on [page 4](#) were measured. The raw data for these measurements is provided in [Table 13](#). The data reduced to deltas in the parameters across the grouping of four irradiations is presented in [Table 14](#). Again the data gives no indication of any damage due to the irradiations.

TABLE 11. SUPPLY AND COMMON MODE CURRENT MONITOR VALUES FOR SEB IRRADIATIONS AT V_{CC} = 5.5V AND V_{CM} = ±20V

IRRADIATION CONDITION		DUT1		DUT2		DUT3		DUT4	
		ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)	ICC (mA)	ICM (mA)
V _{CC} = 0 V _{CM} = -20V	Pre		0.0087		0.0087		0.0087		0.0086
	Post		0.0087		0.0087		0.0086		0.0086
V _{CC} = 0 V _{CM} = +20V	Pre		0.0085		0.0085		0.0085		0.0085
	Post		0.0085		0.0085		0.0085		0.0085
V _{CC} = 5.5V V _{CM} = -20V Slow 50kHz	Pre	7.356	67.062	6.846	66.671	6.966	66.610	7.365	67.150
	Post	7.075	66.497	6.633	66.260	6.863	66.340	7.222	66.879
V _{CC} = 5.5V V _{CM} = +20V Slow 50kHz	Pre	92.701	87.912	92.730	88.115	91.950	87.360	92.781	88.070
	Post	94.350	89.120	93.872	88.952	92.620	87.823	93.370	88.493

September 2015 Addendum Conclusions

From this additional testing it is concluded that the ISL72027SEH did not suffer any damage when operated with V_{CC} = 5.5V and V_{CM} = ±20V and irradiated with ions having LET of 60MeV • cm²/mg. The irradiations were carried out with the part at ambient of approximately +25°C and each irradiation was taken to 1x10⁷ ion/cm².

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TABLE 12. SUPPLY AND COMMON MODE CURRENT DELTAS FOR SEB IRRADIATIONS AT $V_{CC} = 5.5V$ AND $V_{CM} = \pm 20V$

IRRADIATION CONDITION $V_{CC} = 5.5V$	DUT1		DUT2		DUT3		DUT4	
	ICC DELTA (%)	ICM DELTA (%)	ICC DELTA (%)	ICM DELTA (%)	ICC DELTA (%)	ICM DELTA (%)	ICC DELTA (%)	ICM DELTA (%)
$V_{CC} = 0$ $V_{CM} = -20V$		0.0		0.0		-1.1		0.0
$V_{CC} = 0$ $V_{CM} = +20V$		0.0		0.0		0.0		0.0
$V_{CC} = 5.5V$ $V_{CM} = -20V$ Slow 50kHz	-3.8	-0.8	-3.1	-0.6	-1.5	-0.4	-1.9	-0.4
$V_{CC} = 5.5V$ $V_{CM} = +20V$ Slow 50kHz	1.8	1.4	1.2	0.9	0.7	0.5	0.6	0.5

TABLE 13. PARAMETRIC MONITORS FOR EACH SET OF IRRADIATIONS

		ICM (μA) AT $V_{CM} = -7V$	ICM (μA) AT $V_{CM} = +12V$	V_{REF} AT V_{CM} (V)	ICC (mA) UNLOADED FAST	ICC (mA) LOADED SLOW
DUT1	Pre	682	736	1.775	4.315	23.820
	Post	675	731	1.774	4.293	23.793
DUT2	Pre	683	735	1.775	4.292	22.870
	Post	677	729	1.773	4.276	22.734
DUT3	Pre	683	736	1.775	4.314	23.400
	Post	671	726	1.773	4.297	23.398
DUT4	Pre	684	737	1.775	4.332	23.535
	Post	674	728	1.774	4.312	23.521

NOTE: Refer to [Table 10 on page 16](#). Irradiation was with Pr at 0° incidence for effective LET of $60MeV \cdot cm^2/mg$ and each SET of irradiations having a total of $4 \times 10^7 ion/cm^2$.

TABLE 14. DELTAS OF PARAMETRIC MONITORS FOR EACH SET OF IRRADIATIONS

	ICM (μA) AT $V_{CM} = -7V$ (%)	ICM (μA) AT $V_{CM} = +12V$ (%)	V_{REF} AT V_{CM} (V) (%)	ICC (mA) UNLOADED FAST (%)	ICC (mA) Loaded Slow (%)
DUT1	-1	-1	0	-1	0
DUT2	-1	-1	0	0	-1
DUT3	-2	-1	0	0	0
DUT4	-1	-1	0	0	0

NOTE: Refer to [Table 10 on page 16](#). irradiation was with Pr at 0° incidence for effective LET of $60MeV \cdot cm^2/mg$ and each SET of irradiations having $4 \times 10^7 ion/cm^2$.

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